

Novel Noise Liner Development Enabled by Advanced Manufacturing Project 79

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Project manager: Pierre Mulgrave, FAA

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Project 79

Novel Noise Liner Development
Enabled by Advanced Manufacturing



The Pennsylvania State University

PI: Nicholas Meisel

PM: Pierre Mulgrave

Cost Share Partner(s): RTX Technology Research Center, Altair Engineering, Cornerstone Research Group

Objective:

Develop and demonstrate a methodology for rapid design, analysis, fabrication, and testing of novel structure that can enhance noise attenuation in aircraft engines

Project Benefits:

Novel acoustic liner designs and materials will provide a new approach for aircraft engine manufacturers to realize simultaneous noise, emissions, and fuel burn reductions

Research Approach:

- 1. Establish a set of acoustic requirements for future aircraft engine designs
- 2. Design and analyze lattice-based acoustic liners using advanced software tools
- 3. Perform rapid, iterative prototyping and testing to identify promising designs and materials
- 4. Conduct detailed assessments of manufacturability
- 5. Perform acoustic and structural evaluations of novel liners
- 6. Document results and archive data for the FAA

Major Accomplishments (to date):

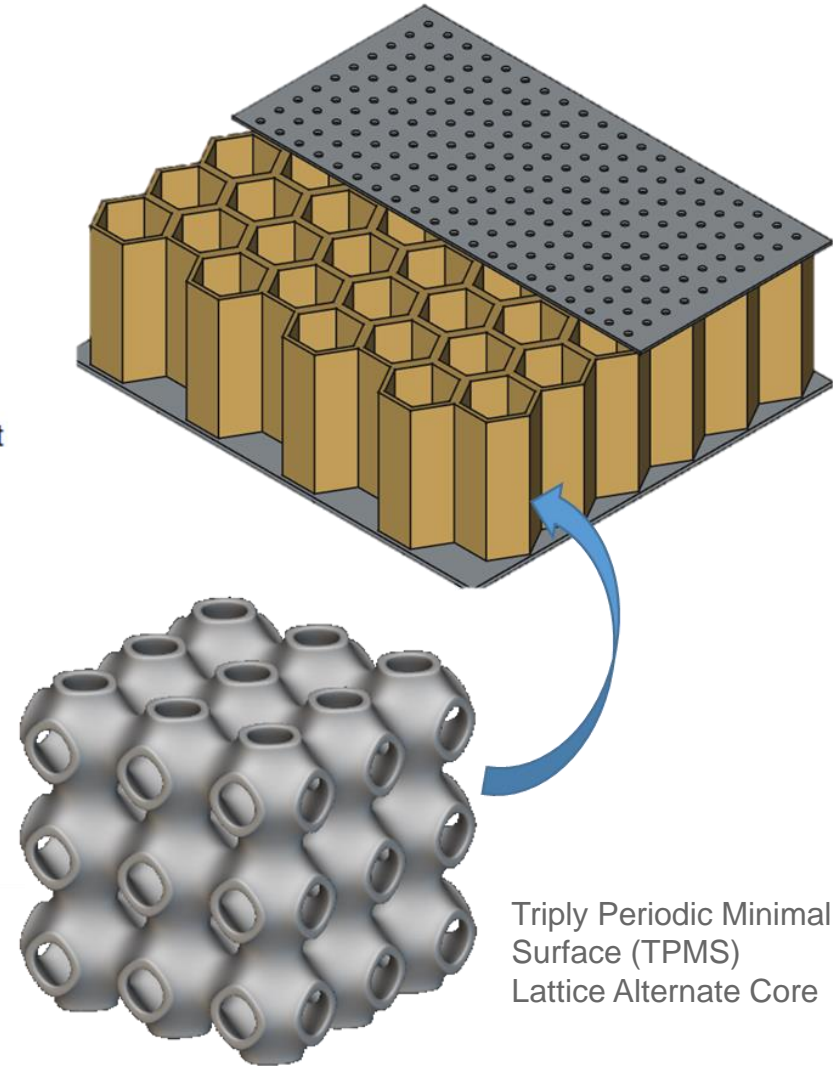
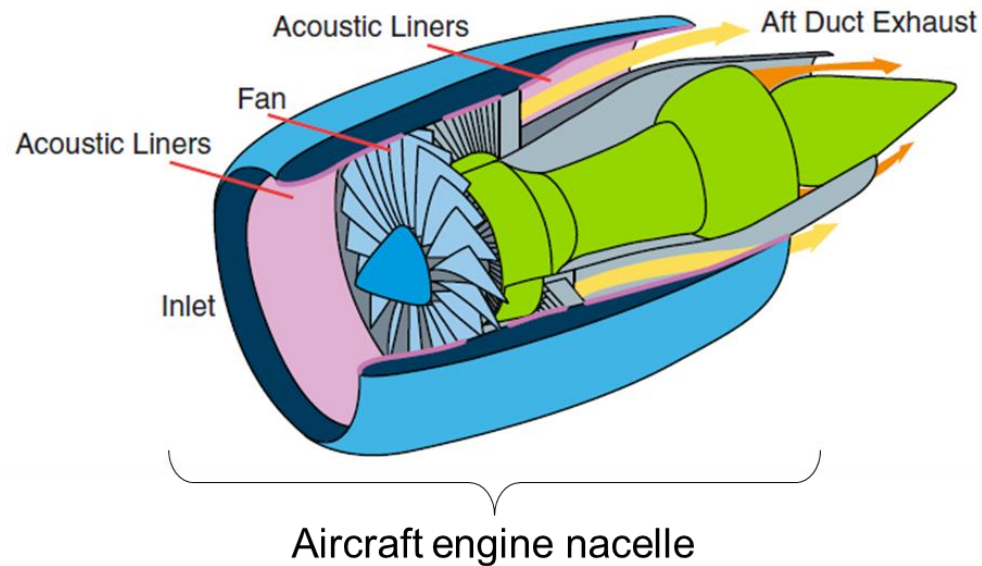
- 1. Computational comparison of a variety of liner designs along with sensitivity analysis of underlying variables
- 2. Established method for quantifying and accounting for manufacturing variations

Future Work / Schedule:

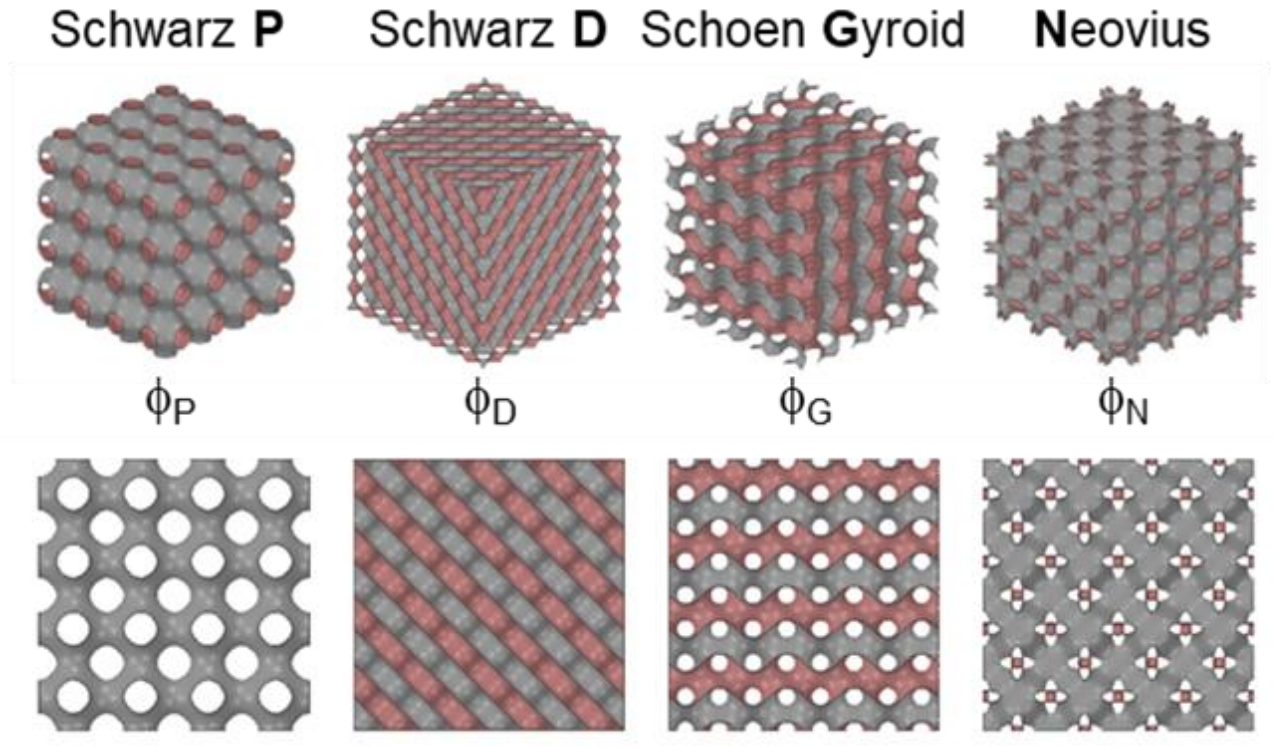
- October 2025: Manufacturing Error Model
- November 2025: Automated Meshing Capabilities
- February 2025: Demonstrating Two Liner Designs
- March 2025: Documentation and Data Archiving
- April 2025: Transition to Metal AM

Acoustic liners are placed in the nacelle of aircraft to reduce noise

Novel acoustic liner designs are needed to address the noise profile of modern engine designs, while meeting space and weight constraints.



To show viability, a comparison against traditional liners is needed



$$\phi_P = \cos(x) + \cos(y) + \cos(z) = C$$

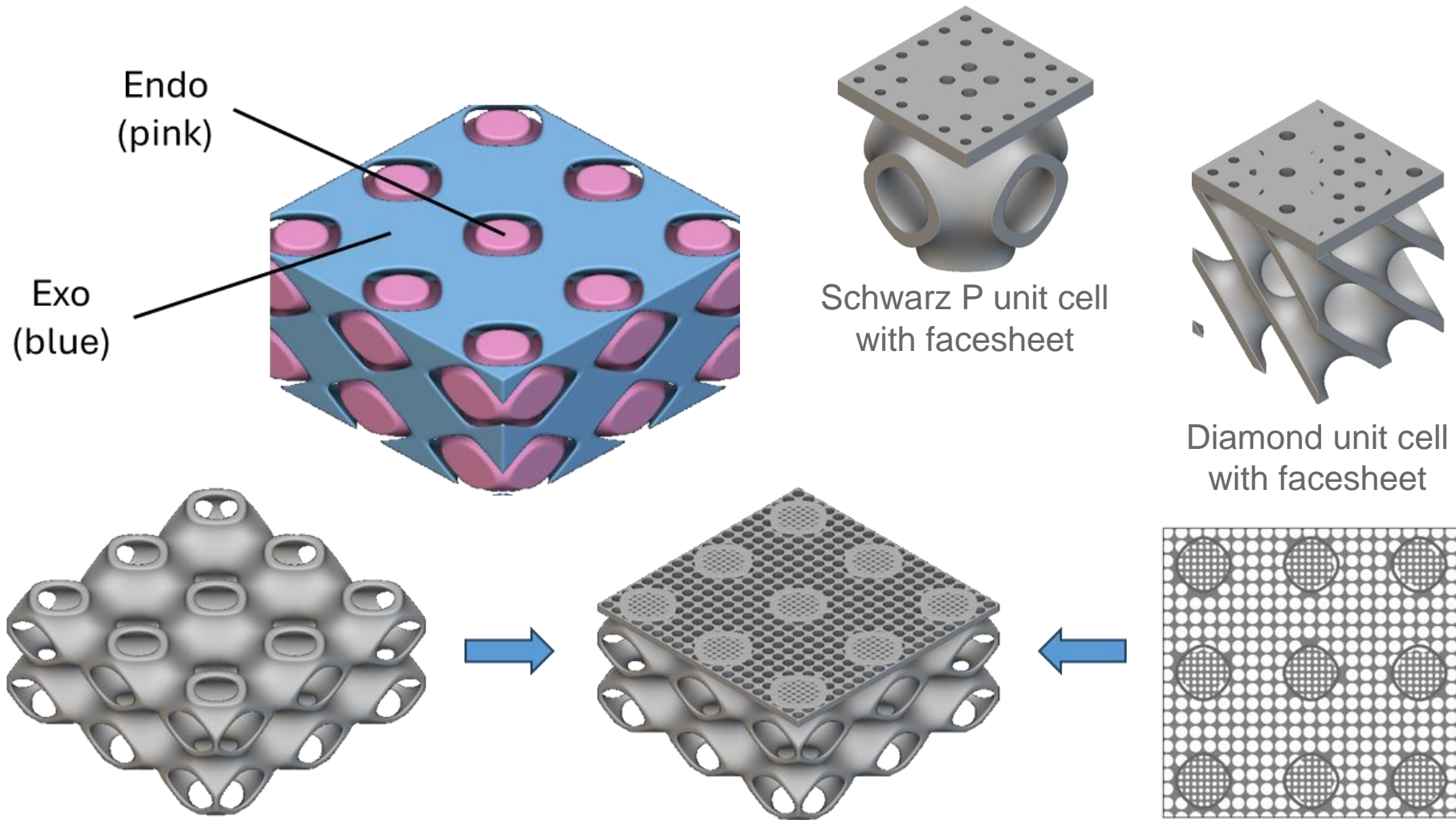
$$\phi_D = \cos(x)\cos(y)\cos(z) - \sin(x)\sin(y)\sin(z) = C$$

$$\phi_G = \sin(x)\cos(y) + \sin(y)\cos(z) + \sin(z)\cos(x) = C$$

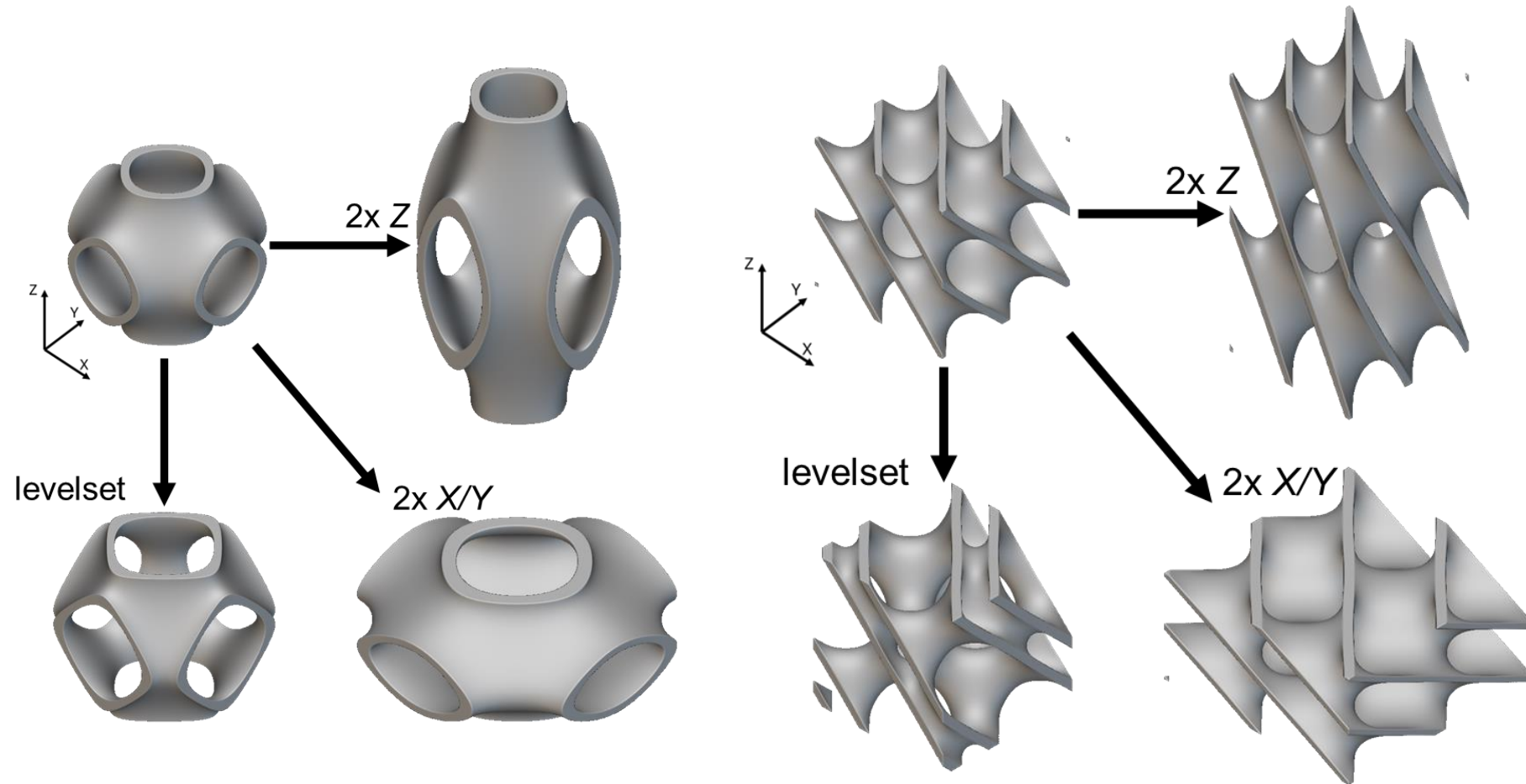
$$\phi_N = 3[\cos(x) + \cos(y) + \cos(z)] + 4\cos(x)\cos(y)\cos(z) = C$$



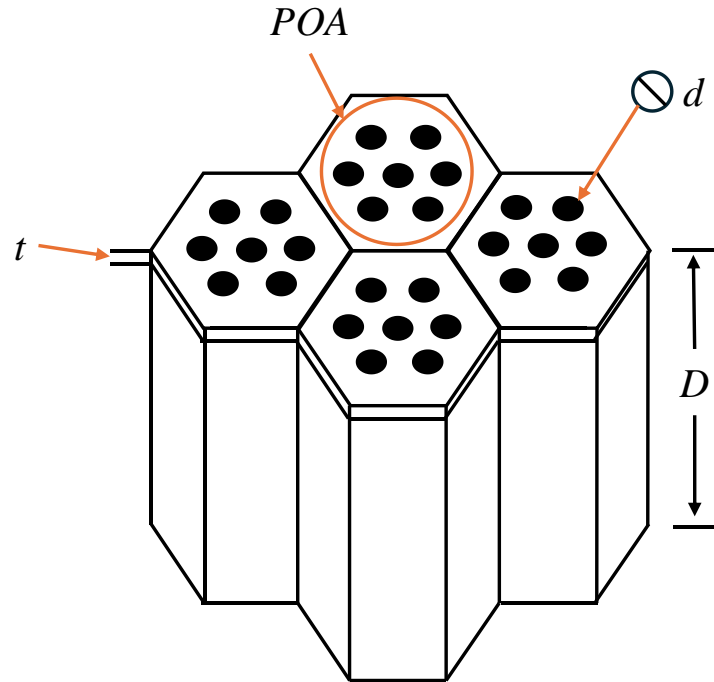
TPMS Lattices include two intersecting fluid regions along with a facesheet



The design of TPMS structures can be adjusted through certain variables

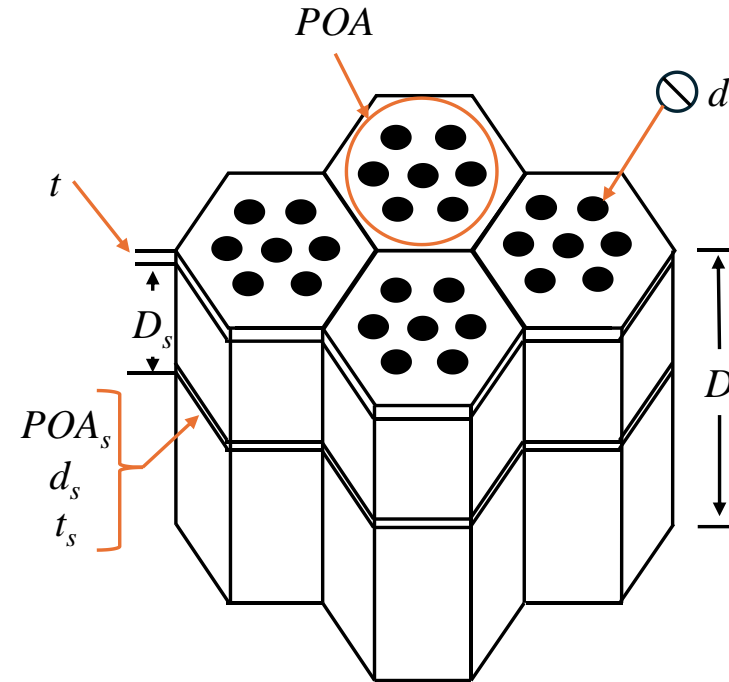


This contrasts with current honeycomb-based liners



Single Degree of Freedom (SDOF)

- Honeycomb core
- Perforated facesheet



Double Degree of Freedom (DDOF)

- Honeycomb core
- Perforated facesheet
- Perforated septum

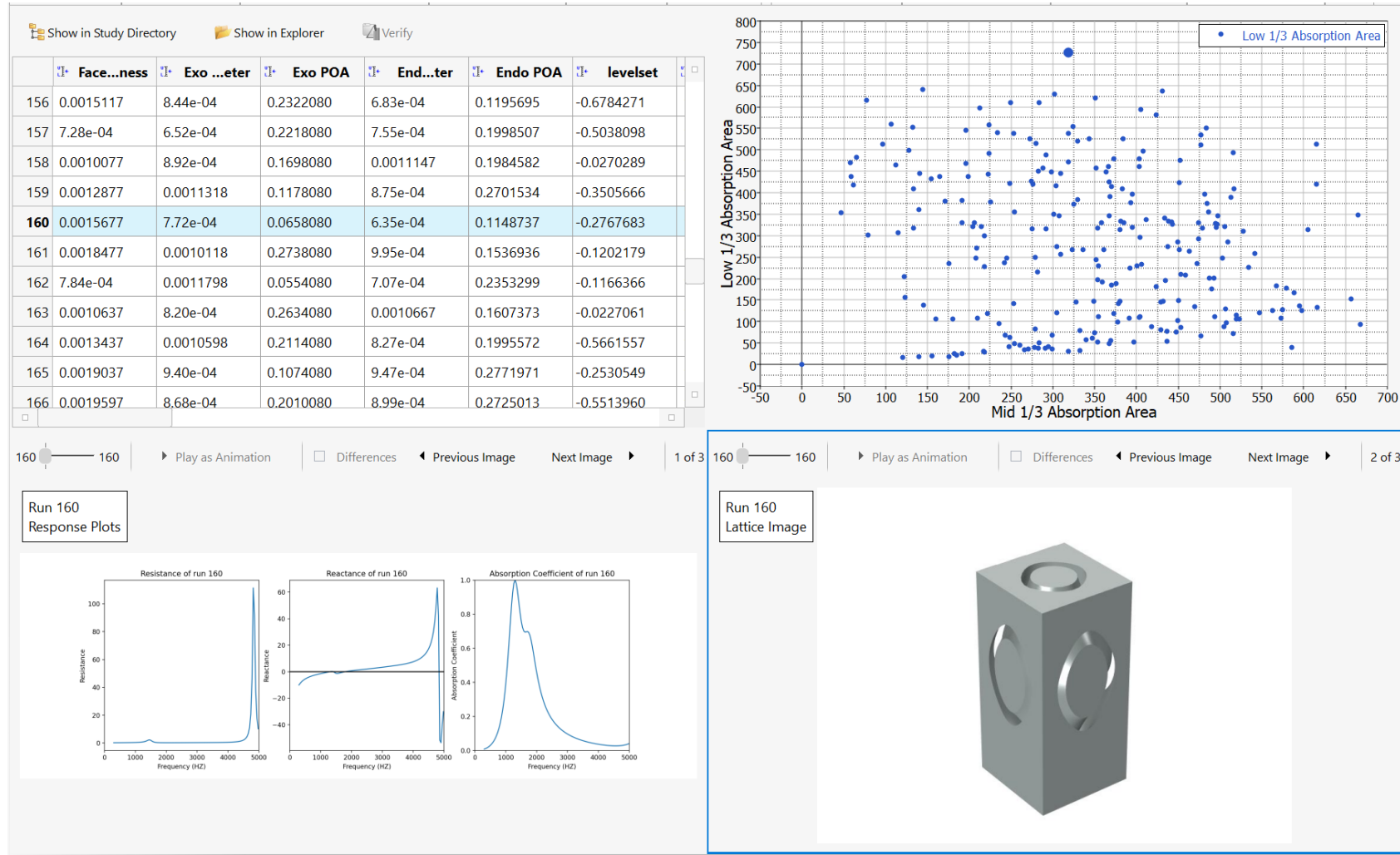


We need to understand the impact of each variable on performance

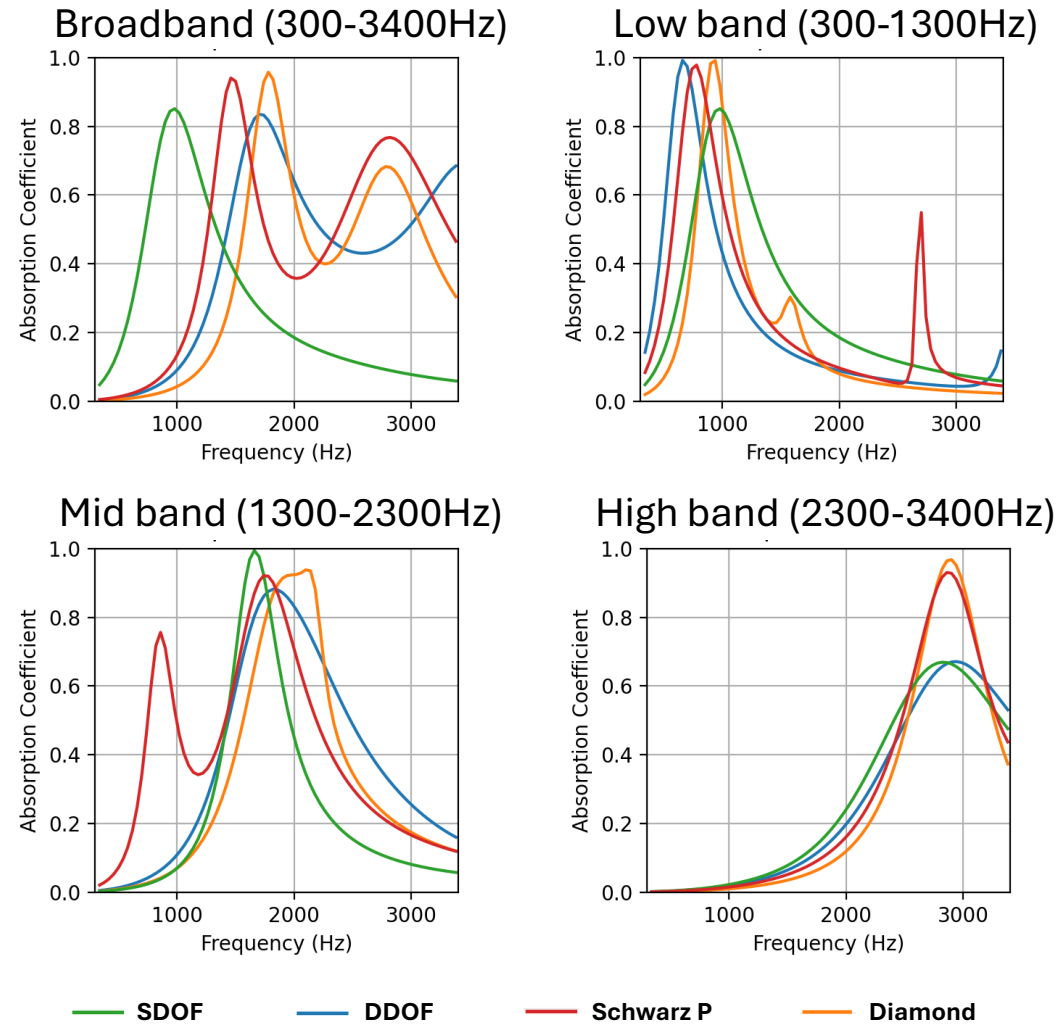
SDOF	DDOF	TPMS
# of Facesheet Perforations	# of Facesheet Perforations	X/Y Unit Cell Size
Perforation Diameter	Perforation Diameter	Z Unit Cell Size
Facesheet Thickness	Facesheet Thickness	Z: # of Cells
Liner Depth	Liner Depth	Levelset (Facesheet)
	# of Septum Perforations	Levelset (Backplate)
	Septum Perf. Diameter	Facesheet Thickness
	Septum Thickness	Endo Perf. Diameter
	Septum Depth	# of Endo Perforations
		Exo Perf. Diameter
		# of Exo Perforations



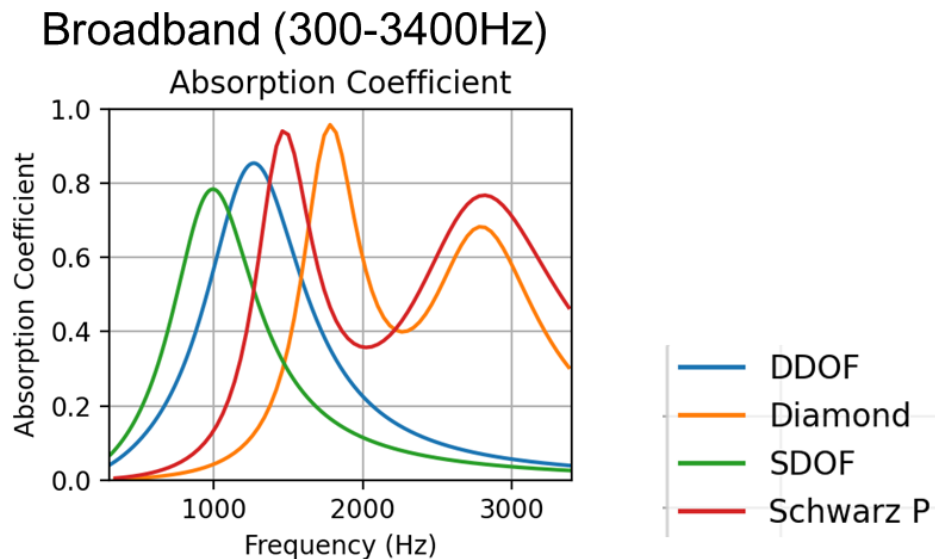
Variables were used in a DOE via the dashboard discussed last year



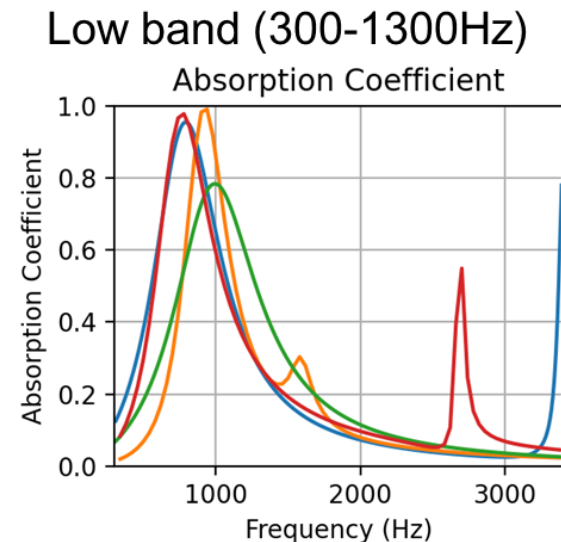
COMSOL shows top TPMS designs matching or exceeding honeycombs



Findings show that top TPMS designs require less depth than honeycombs



Liner Type	Depth (mm)
SDOF	36.0 mm
DDOF	24.0 mm
Schwarz P	11.9 mm
Diamond	11.6 mm

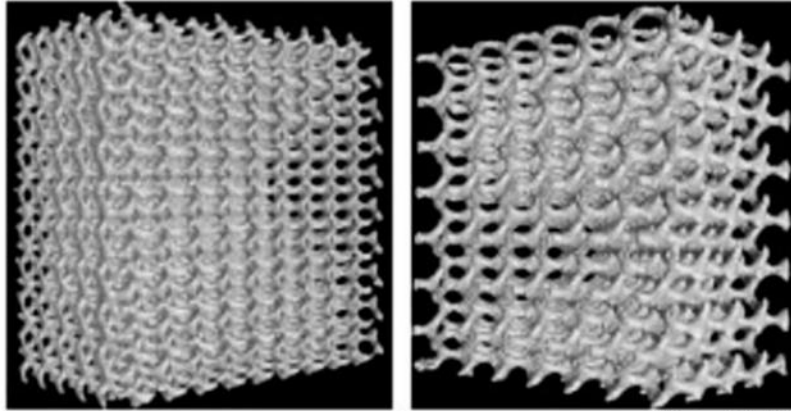


Liner Type	Depth (mm)
SDOF	36.0 mm
DDOF	38.0 mm
Schwarz P	27.1 mm
Diamond	18.7 mm



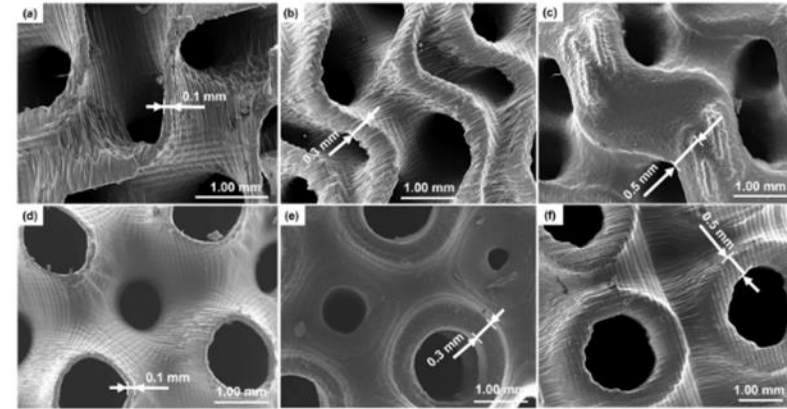
While the performance is promising, we need ways of evaluating quality

X-ray Computed Tomography (XCT)



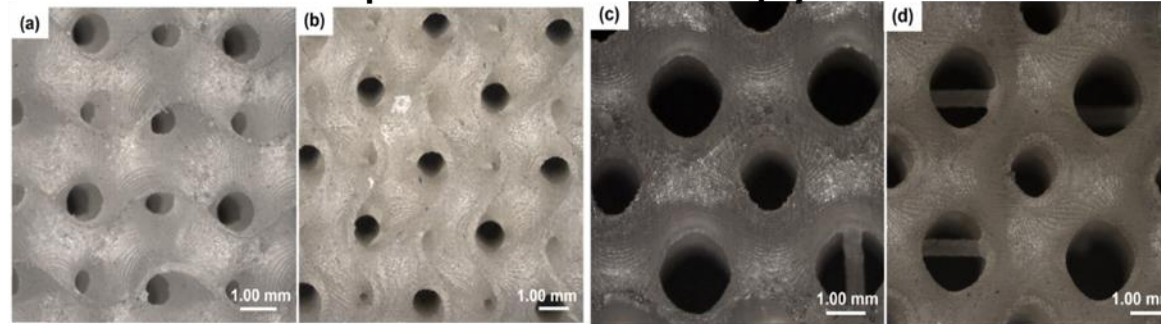
Yan 2012

Scanning Electron Microscopy



Gabrieli 2024

Optical Microscopy



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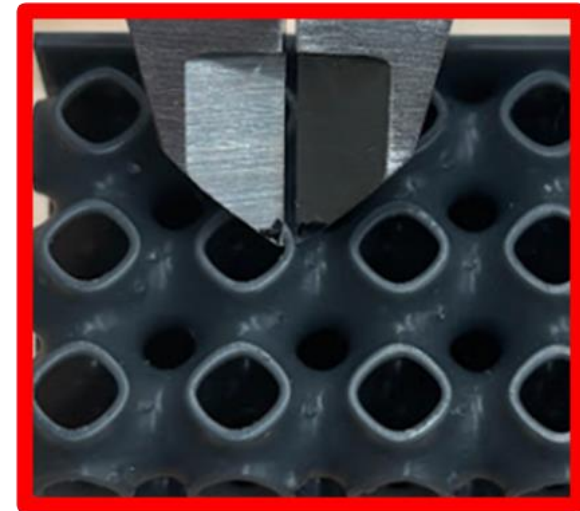
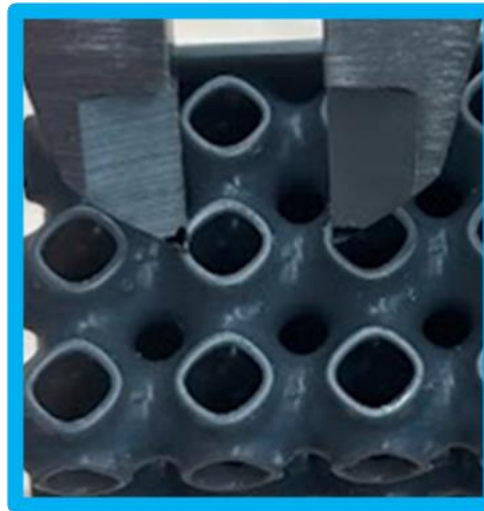
As an alternative, we're developing low-cost methods for quality checks

Manual Measurement Method	Automated Screening Method
<ul style="list-style-type: none">• Uses a combination of physical measurements and image analyses.• Provides direct quantitative data on the dimensions of several design variables.• Measured distributions can be used to evaluate the stochastic error within the parts.• The results can be used to make design adjustments and dial in the manufactured dimensions.	<ul style="list-style-type: none">• Uses image processing and analysis along with machine learning to evaluate several geometric characteristics.• Outputs the total number of print defects based on user defined pass/fail criteria.• Can be used to quickly judge the quality of a finished printed part and determine whether a new print is necessary.



Our manual methods are focusing on standardized use of calipers

Measurement Tool	Variable	Measurement Technique
Digital calipers	Face Sheet Thickness	Measure the thickness around the edge of the face sheet.
	Unit Cell Size	Measure the offset unit cell size by finding the distance from the pore edge of one cell to the corresponding pore edge of an adjacent cell.
	Wall Thickness	Measure the wall thickness around the exposed lattice pore edges.



Measurements are grouped by orientation as taken from the lattice

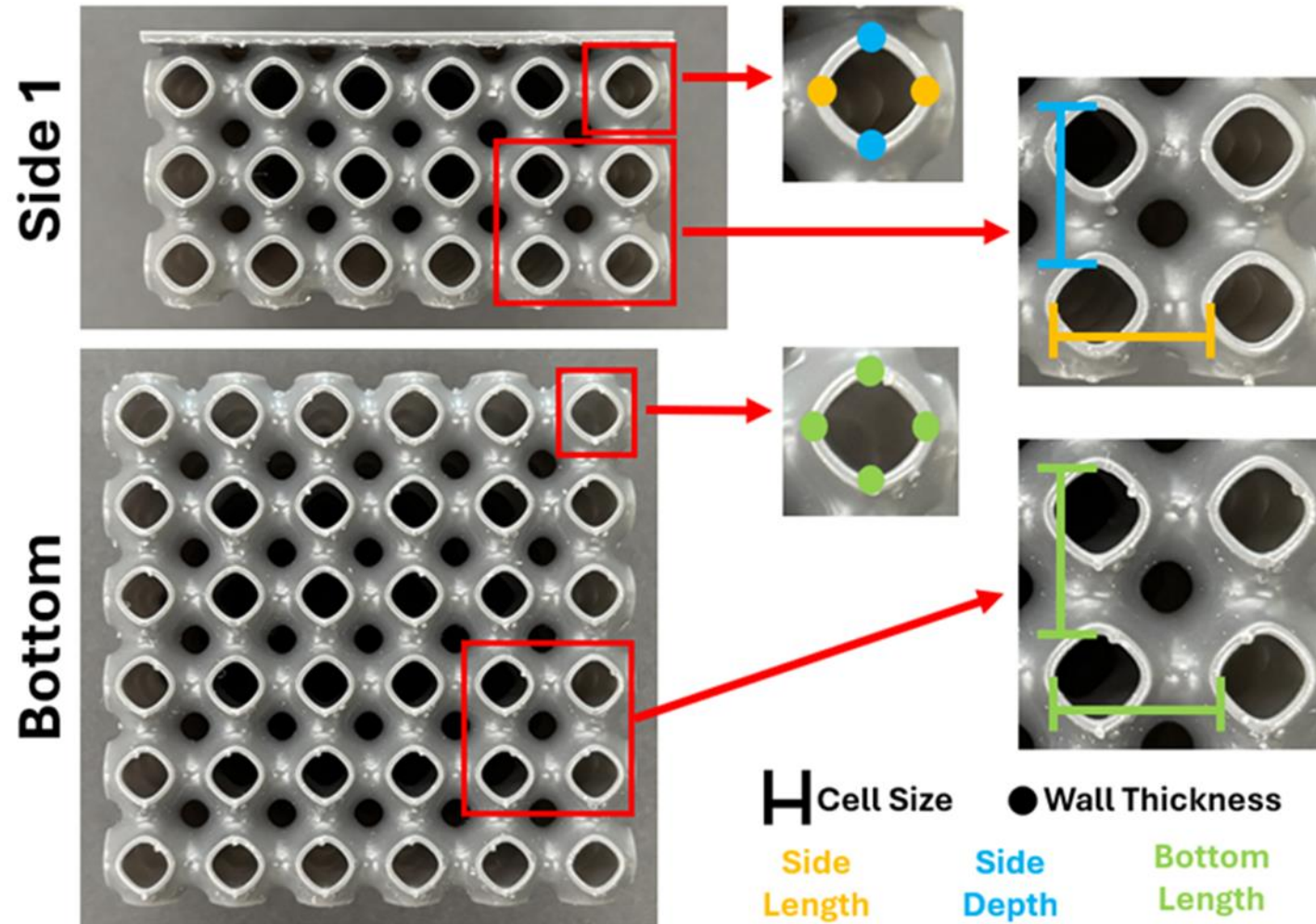
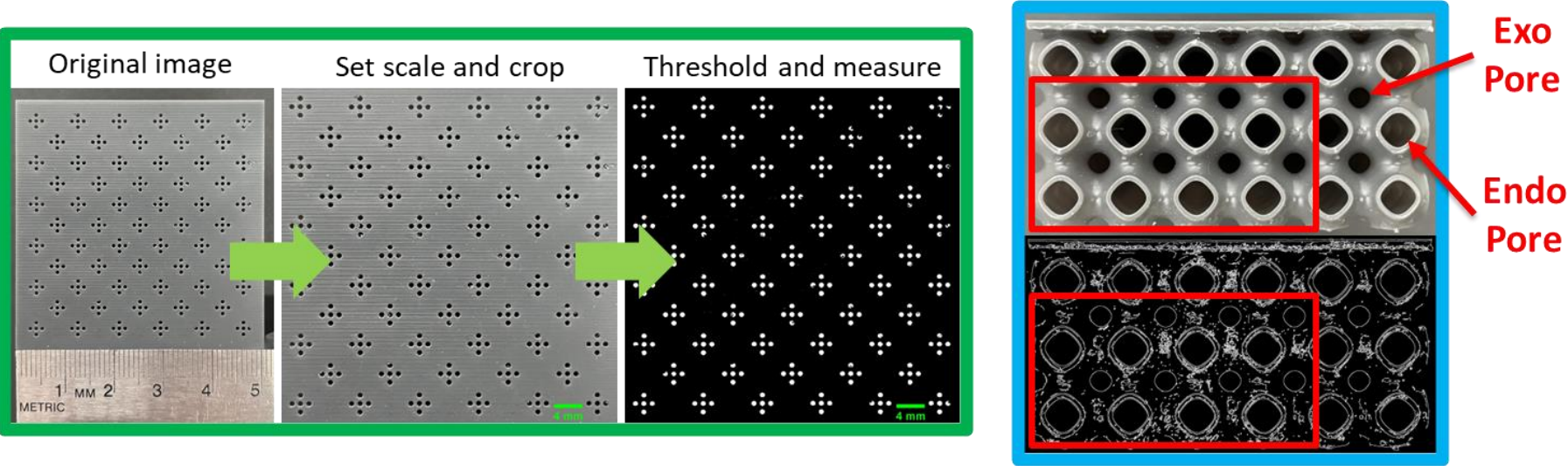
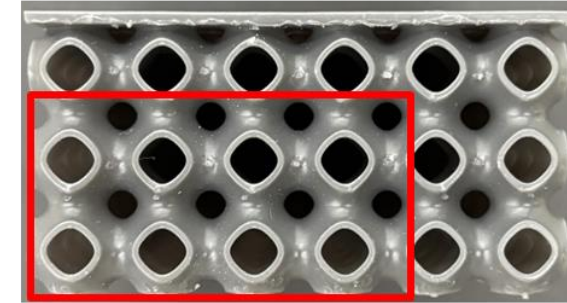
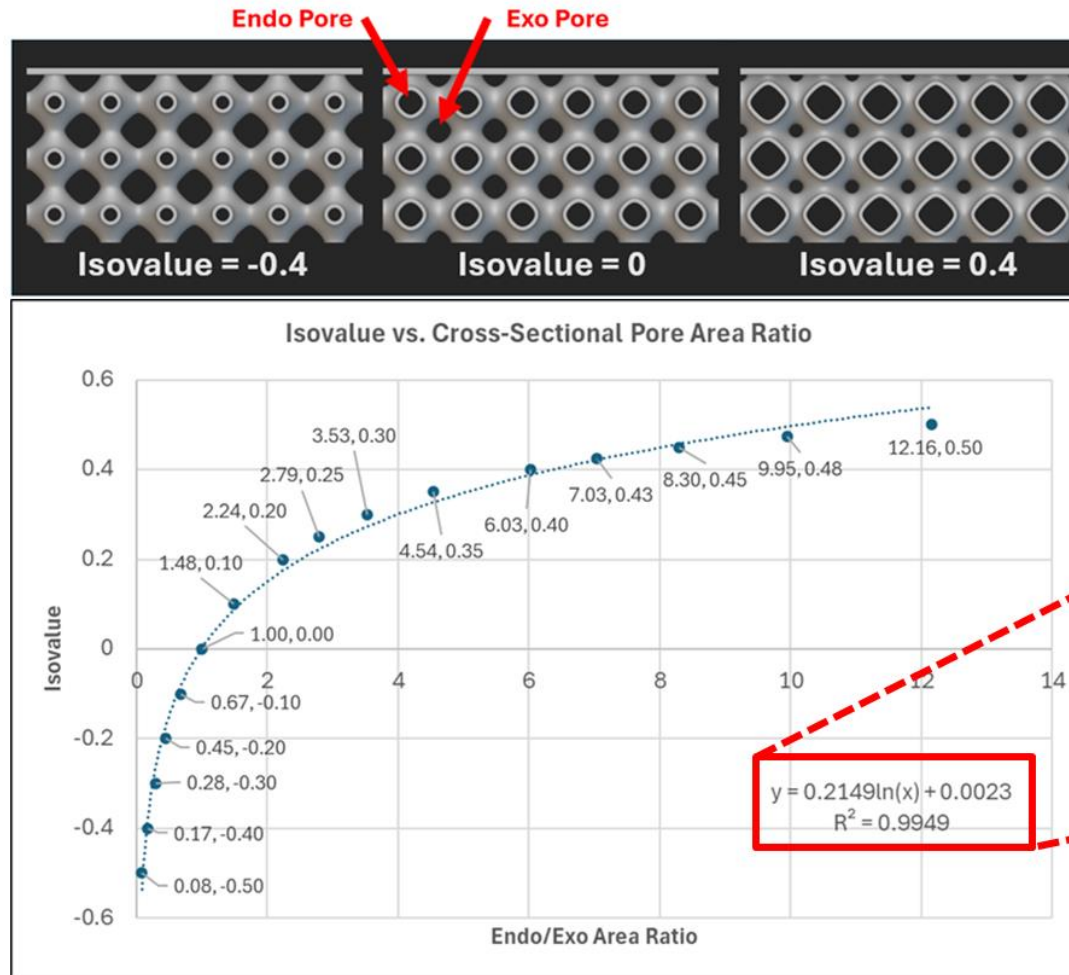


Image processing tools also support manual data collection

Measurement Tool	Variable	Measurement Technique
Adobe Lightroom and ImageJ	Perforation Diameter	Threshold images of the face sheet so only the perforations are visible. Batch measure the areas of the perforations. Use the areas to estimate the diameter of the perforation.
	Percent open area	Threshold images of the face sheet so only the perforations are visible. Find the total area of the perforations and divide it by the total area of the face sheet.
	Isovalue	Use edge detection to capture clean edges of the lattice pores. Find the cross-sectional area ratio between the corresponding endo and exo pores. Convert the ratios to isovalues using an isovalue vs. area ratio relationship calculated from the ideal model.



Lattice pore area ratios helped to generate a relationship to isovalues



This equation can be used to estimate the isovalue given the endo/exo pore area ratio.

$$y = 0.2149\ln(x) + 0.0023$$
$$R^2 = 0.9949$$



From these measurements, certain key issues are identified

- All manufactured variables that define solid features were found to be oversized from their nominal dimensions.
- Perforation Diameter, and therefore percent open area, were found to be undersized since they dictate negative features.
- Wall thickness measured along the depth of the core was found to print thicker.
- For some variables, the nominal dimension fell outside the measured range.

Variable	Nominal	Average	Standard Deviation	Minimum	Maximum
Face Sheet Thickness	1 mm	1.17 mm	0.05 mm	1.09 mm	1.29 mm
Unit Cell Size (Side Length)	8.47 mm	8.51 mm	0.04 mm	8.43 mm	8.61 mm
Unit Cell Size (Side Depth)	8.47 mm	8.51 mm	0.05 mm	8.42 mm	8.59 mm
Unit Cell Size (Bottom Length)	8.47 mm	8.50 mm	0.04 mm	8.42 mm	8.59 mm
Wall Thickness (Side Length)	0.6 mm	0.64 mm	0.03 mm	0.55 mm	0.71 mm
Wall Thickness (Side Depth)	0.6 mm	0.73 mm	0.05 mm	0.64 mm	0.87 mm
Wall Thickness (Bottom Length)	0.6 mm	0.63 mm	0.04 mm	0.55 mm	0.72 mm
Perforation Diameter	0.8 mm	0.69 mm	0.02 mm	0.64 mm	0.72 mm
Percent Open Area (POA)	5.94%	4.26%	N/A	N/A	N/A
Isovalue	0.2	0.201	0.003	0.192	0.207



A multidisciplinary team has ensured the innovative potential of the project



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